

EVOLUTION

Incinerator → TDP

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Date: 09th Aug 2023



MY BACKGROUND

WASTE MANAGEMENT

Phuket 700TPD MSW Incineration Power Plant



China 300TPD MSW to Fertilizer Plant



Malaysia 100TPD SW Incineration Power Plant



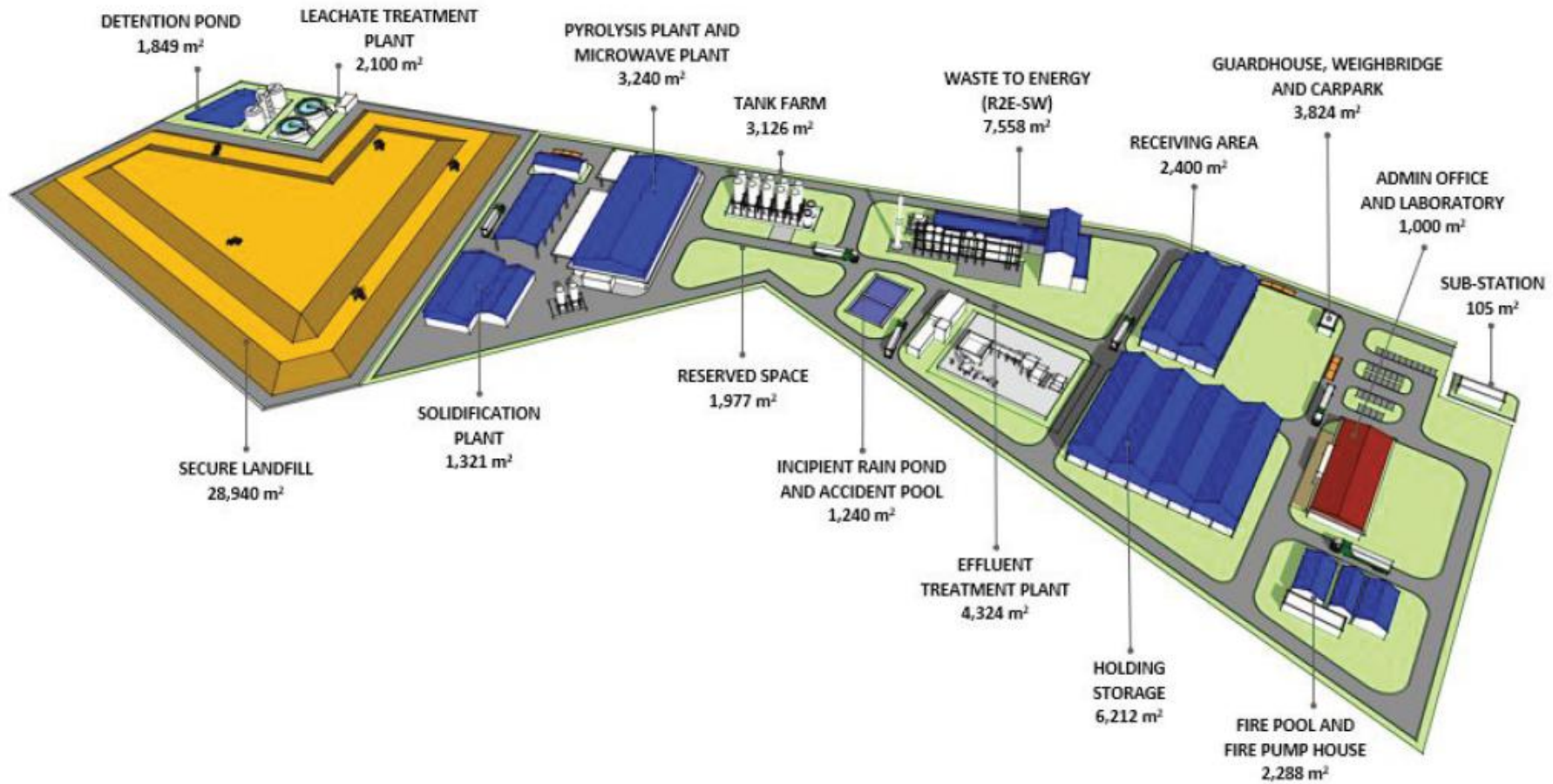
Surabaya 750TPD MSW Incineration Power Plant



Malaysia

3rd SW Treatment Centre

CONCEPTUAL DESIGN





CHALLENGES

FACED BY POM

Empty Fruit Bunches



Wet Decanter Cake



EQ CAR 2014

Obligation to comply

4. (2) An owner of every existing premises, including that which is not subject to any condition on limit values for air pollutants whether on the licence issued or approval granted for the operation of the existing facility, shall, on or before the expiry of five years from the date on which these Regulations come into operation, take such measures as may be necessary to comply with the opacity and limit values as specified in regulations 12 and 13.

Made 23 April 2014
[AS(U)91/110/611/077]ld. 10; PN(PU2)280/XV]

DATUK SERI PALANIVEL A/L GOVINDASAMY
Minister of Natural Resources and Environment

P.U. (A) 151

 4 Jun 2014 4 June 2014 P.U. (A) 151	WARTA KERAJAAN PERSEKUTUAN <i>FEDERAL GOVERNMENT GAZETTE</i>
PERATURAN-PERATURAN KUALITI ALAM SEKELILING (UDARA BERSIH) 2014 <i>ENVIRONMENTAL QUALITY (CLEAN AIR) REGULATIONS 2014</i>	

EQ CAR 2014

SECOND SCHEDULE

[Regulation 13]

LIMIT VALUES AND TECHNICAL STANDARDS (GENERAL)

(I) Control of fuel burning equipment, incinerators and crematoria

1. Control of fuel quality for fuel burning equipment and incinerators not covered by the First Schedule:

Fuel type	Fuel	Fuel quality parameter
Liquid	All	Sulphur content < 500 ppm (per weight)
Solid	Coal	Sulphur content < 1% (per weight)
	Biomass	Wood, agricultural waste, etc.: air dry and in its natural composition (e.g. wood without coating, paint or other treatment)
		Residues from wood-based industries: without wood preservatives

EQ CAR 2014

The CO₂ reference content is 12%.

Fuel type	Pollutant	Limit value	Monitoring
Solid	Total particulate matter (PM) Where dust load emitted: (a) > 0.44 < 1.0 kg/h (b) ≥ 1.0 < 1.5 kg/h (c) ≥ 1.5 < 2.0 kg/h (d) ≥ 2.0 < 2.5 kg/h ⁷⁰ (e) ≥ 2.5 kg/h	150 mg/m ³	Once/year 2 times/year 3 times/year 4 times/year Continuous*
	Carbon monoxide (CO)	1000 mg/m ³	Periodic

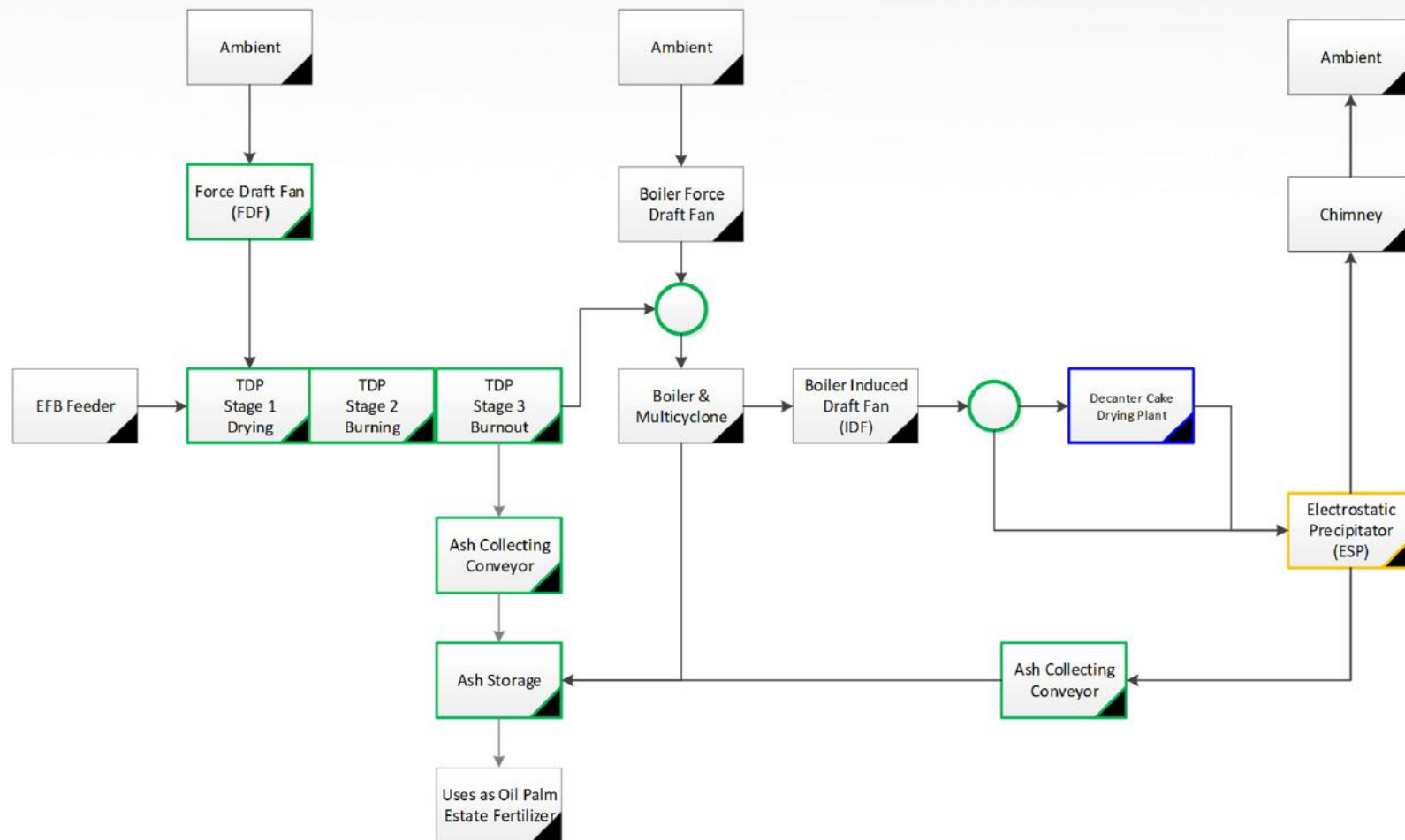
*Averaging time for continuous monitoring is 30 minutes



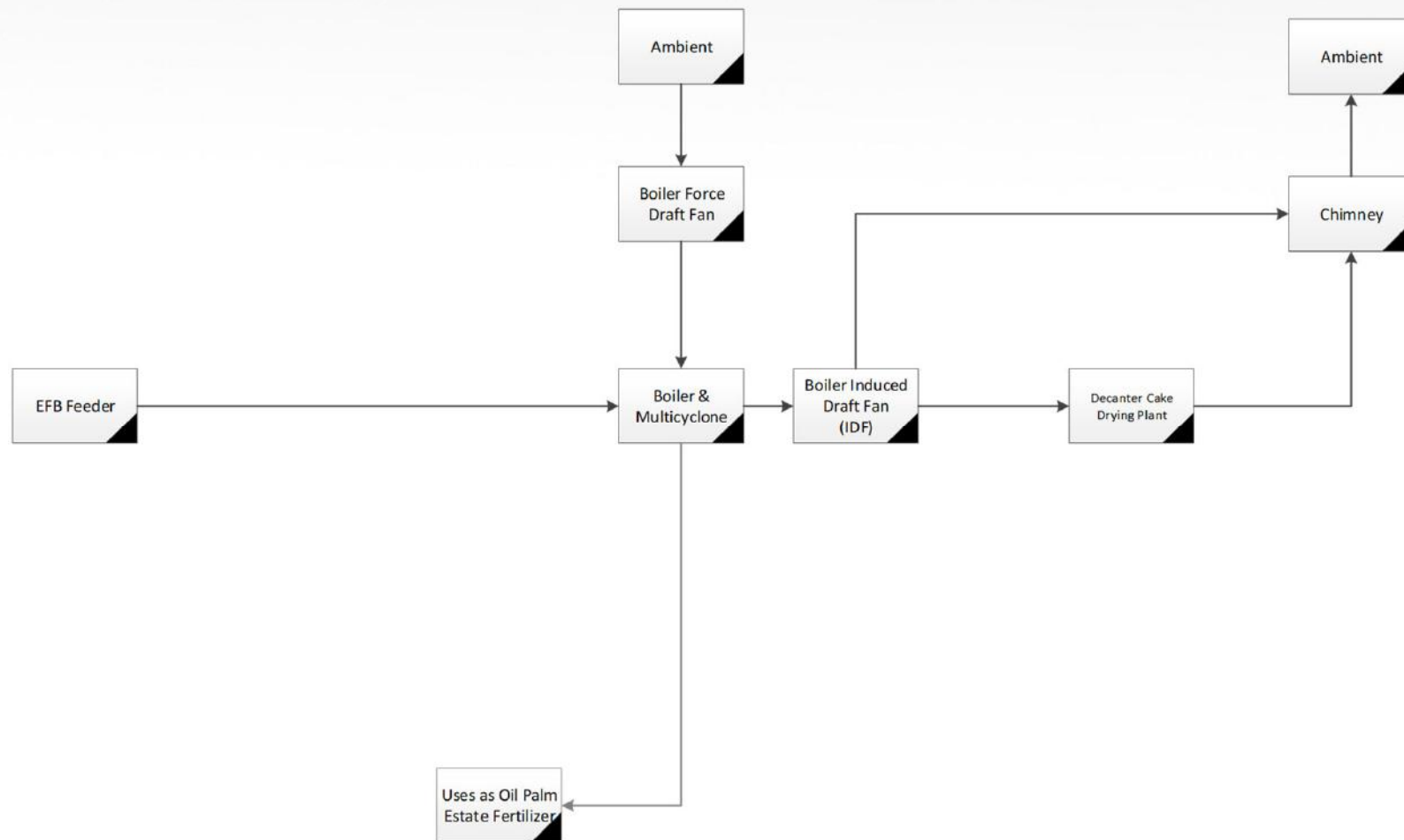
INNOVATION

THERMAL **D**ECOMPOSITION
PLANT

TDP TRIAL @ MJM



ORIGINAL SET UP @ MJM



TDP CALCULATION

1 INPUT

1.1 Ultimate Analysis

Element	C	H	O	N	S	Cl
Percentage	36.97%	5.12%	33.52%	0.34%	0.35%	0.00%

1.2 Proximate Analysis

Element	Moisture	Ash	Combustible	Density	HHV, kJ/kg
Percentage	20.00%	3.70%	76.30%	0.50	14,794

1.3 Throughput				
FFB Throughput	=	70 t/h		
EFB: FFB Ratio	=	23%		
EFB Throughput	=	16.1 t/h (Before press)		
Moisture Content	@	75% [Based on Test Report]		
Throughput	=	4.83 t/h (After drying)		
Moisture Content	@	20% [Design to control]		
	=	4,830 kg/h		

2 CALCULATION

2.1 CALORIFIC VALUE

2.1.1 LHV	=	$81C + 246H + 26S - 26O - 6W$	
	=	3,273 kCal/kg	
	=	13,700 kJ/kg	
Total Heat Output	=	66 GJ/h	

2.1.2 HHV	=	$LHV + 600(W + 9H)$	
	=	3,669 kCal/kg	
	=	15,360 kJ/kg	

< 5%

2.2 AIR REQUIREMENT

2.2.1 Excess air factor	=	1.8
2.2.2 Air Required, L_0	=	$[8.89C + 26.7H + 3.33S - 3.33O] \times 10^{-2}$
	=	3.55 Nm^3/kg
	=	30,867 Nm^3/h

2.2.3 Air Required, L_0	=	$[11.6C + 34.78H + 4.35S - 4.35O] \times 10^{-2}$
	=	4.63 kg/kg
	=	40,236 kg/h

2.3 FLUE GAS

2.3.1 Wet Flue Gas, L_v	=	$(m - 0.21)L_0 + 1.867C + 0.7S + 0.8N + 11.2H + 1.24W + 0.62Cl$
	=	7.16 Nm^3/kg
	=	34,594 Nm^3/h

2.3.2 Air Moisture Content

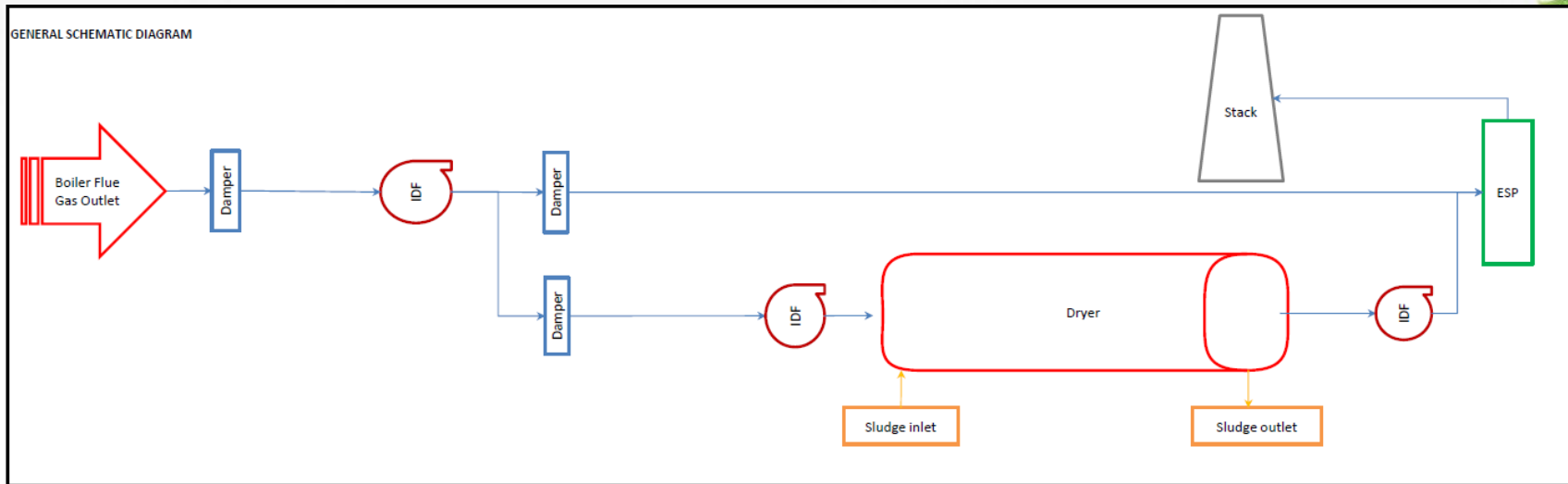
2.3.2.1 Content	=	1.5%
2.3.2.2 L_m	=	0.0959 Nm^3/kg

2.3.3 Dry Flue Gas (Flow)	=	$L_v - L_m - W - 9H$
	=	6.41 Nm^3/kg
	=	30,938 Nm^3/h

2.3.4 Dry Flue Gas (Mass)	=	$(m - 0.2)L_0 + 3.667C + 2S + N + 9H + W + 1.03Cl$
	=	7.71 kg/kg
	=	37,229 kg/h

Normal Condition	
P_1	- Pa
V_1	34,594 Nm^3/h
T_1	0 °C
Actual Condition	
P_2	- Pa
V_2	116,961 m^3/h
T_2	650 °C

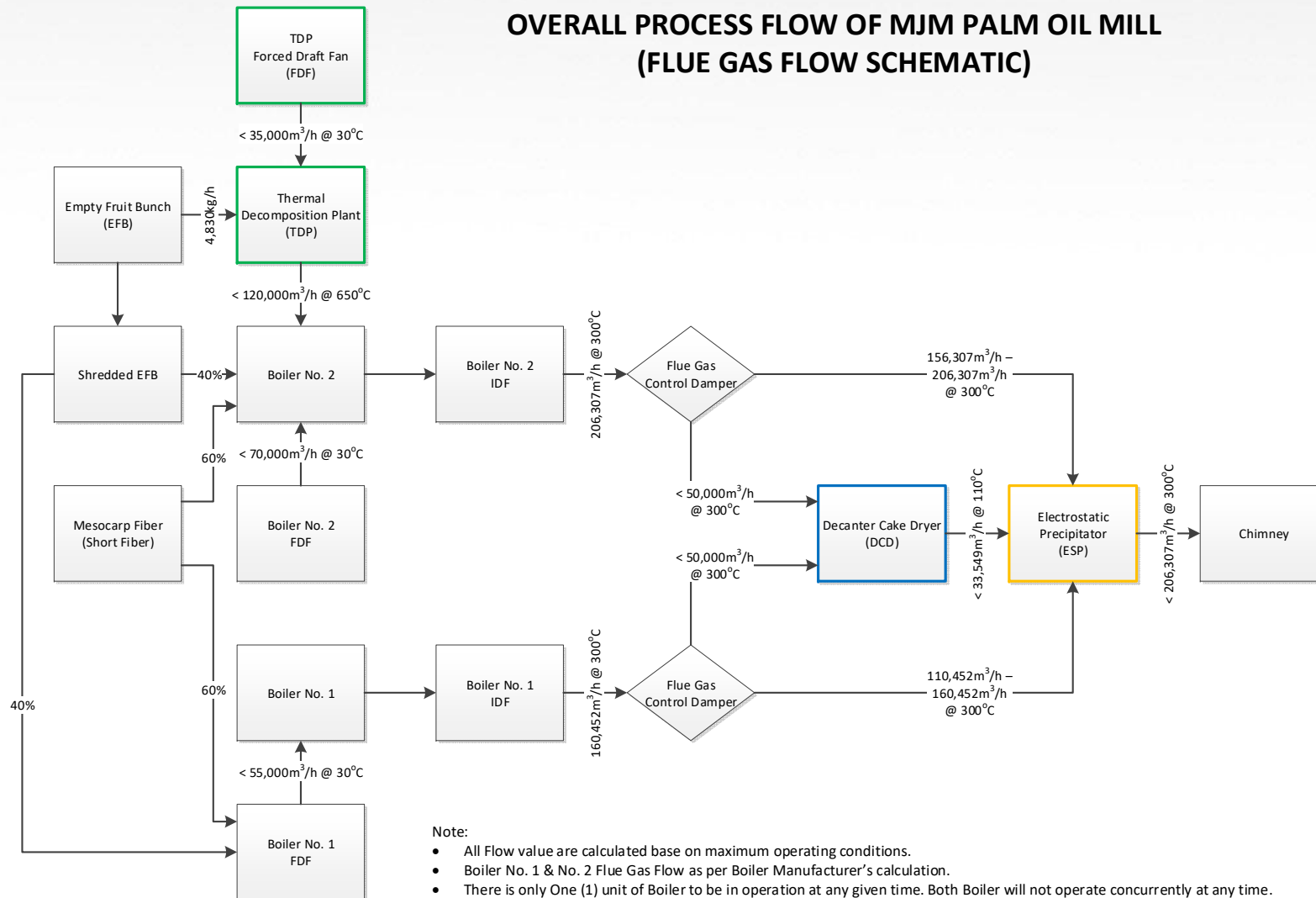
DRYER CALCULATION



SLUDGE DRYING PROCESS		FLUE GAS DRYING PROCESS	
INLET Mass flowrate: 4 t/h Moisture content: 75% Temperature: 40 °C Dry matter flowrate: 1000 kg/h Water content: 3,000 kg/h		INLET Temperature: 300 °C Relative Humidity: 0.20% Enthalpy: 689.778 kJ/kg Humidity Ratio: 125.6609 g/kg Specific Volume: 1.953 m³/kg Moisture per m³ flow: 0.0643 kg/m³	
MASS BALANCE OUTLET Mass flowrate: 1,111 kg/h Moisture content: 10% Temperature: 60 °C Water content: 111 kg/h		MASS BALANCE OUTLET Temperature: 110 °C Relative Humidity: 17.92% Enthalpy: 689.78 kJ/kg Humidity Ratio: 214.28 g/kg Specific Volume: 1.46 m³/kg Moisture per m³ flow: 0.1468 kg/m³ Flow rate required: 35,050 m³/h	
ASSUMPTION Specific heat of water: 4.182 kJ/kg.K Latent heat of water: 2,230 kJ/kg Specific heat of sludge: 0.8 kJ/kg.K		ENERGY BALANCE INLET CONDITION Temperature: 300 °C Specific Energy: 689.778 kJ/kg Relative Humidity: 0.20% Humidity Ratio: 125.6609 g/kg	
ENERGY BALANCE CALCULATION Water evaporated: 2,889 kg/h Energy to heat up water: 9,293 kJ/h Energy to heat up sludge: 16,000 kJ/h Energy to evaporate water: 7,167,102 kJ/h Total energy: 7,192,396 kJ/h		ENERGY BALANCE OUTLET CONDITION Temperature: 110 °C Specific Energy: 689.78 kJ/kg Specific Volume: 1.46 m³/kg Without evaporation: Humidity Ratio: 125.6609 g/kg Enthalpy: 448.85 kJ/kg Net Energy differences: 240.93 kJ/kg Energy per m3 flow: 165.02 kJ/m³ Flow rate required: 43,584 m³/h	
COLOUR NOTES Input Assumption Value from Psychrometric Chart		For Reference Only Temperature: 110 °C, 130 °C Relative Humidity: 20.00%, 9.08% Enthalpy: 782.55, 689.78 kJ/kg Humidity Ratio: 248.82, 204.06 g/kg Specific Volume: 1.52, 1.519 m³/kg Moisture per m³ flow: 0.1637, 0.1343 kg/m³ Flow rate required: 29,077, 41,273 m³/h	

DETAIL SCHEMATIC

OVERALL PROCESS FLOW OF MJM PALM OIL MILL (FLUE GAS FLOW SCHEMATIC)



TDP CONSTRUCTION

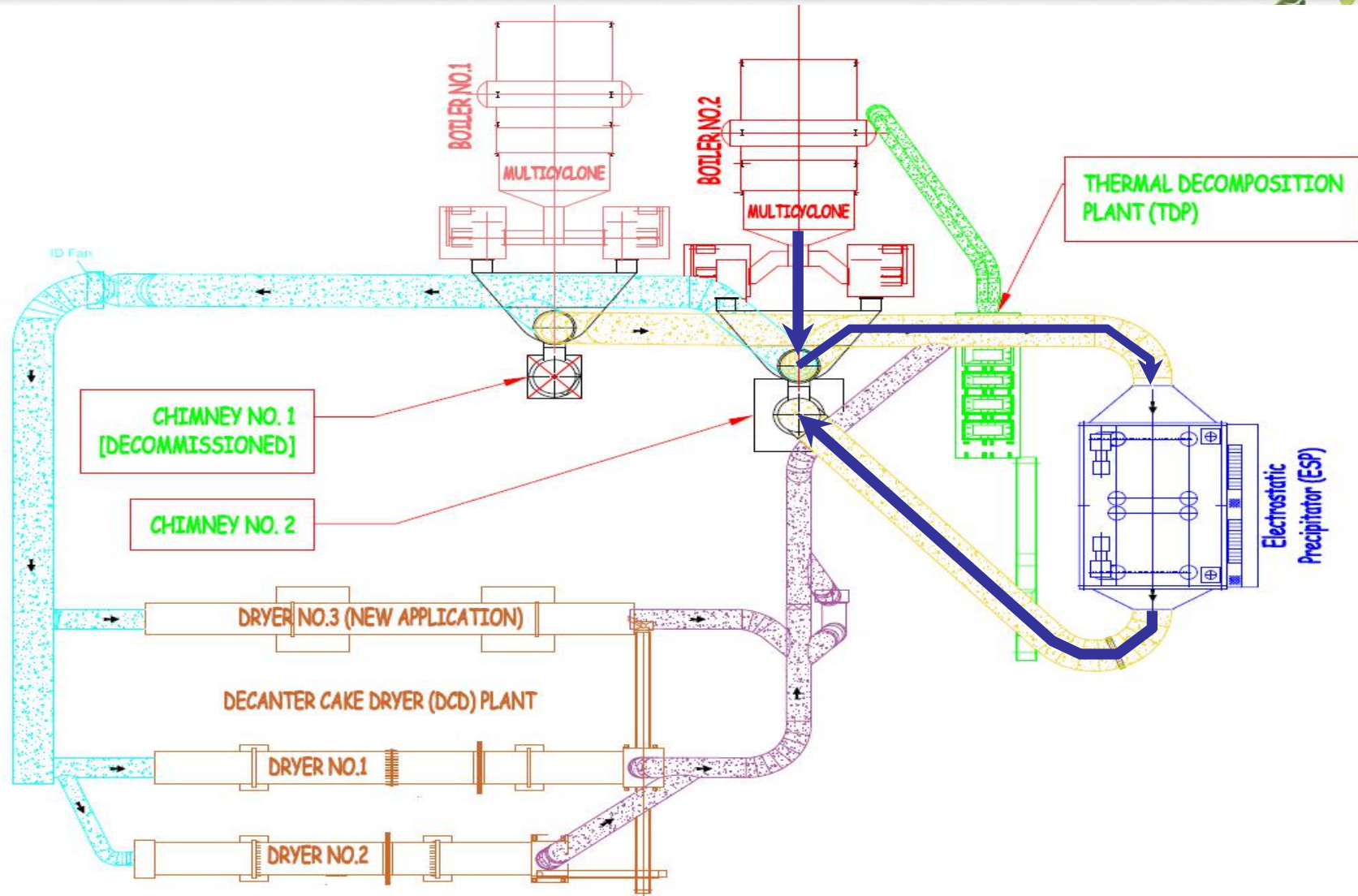




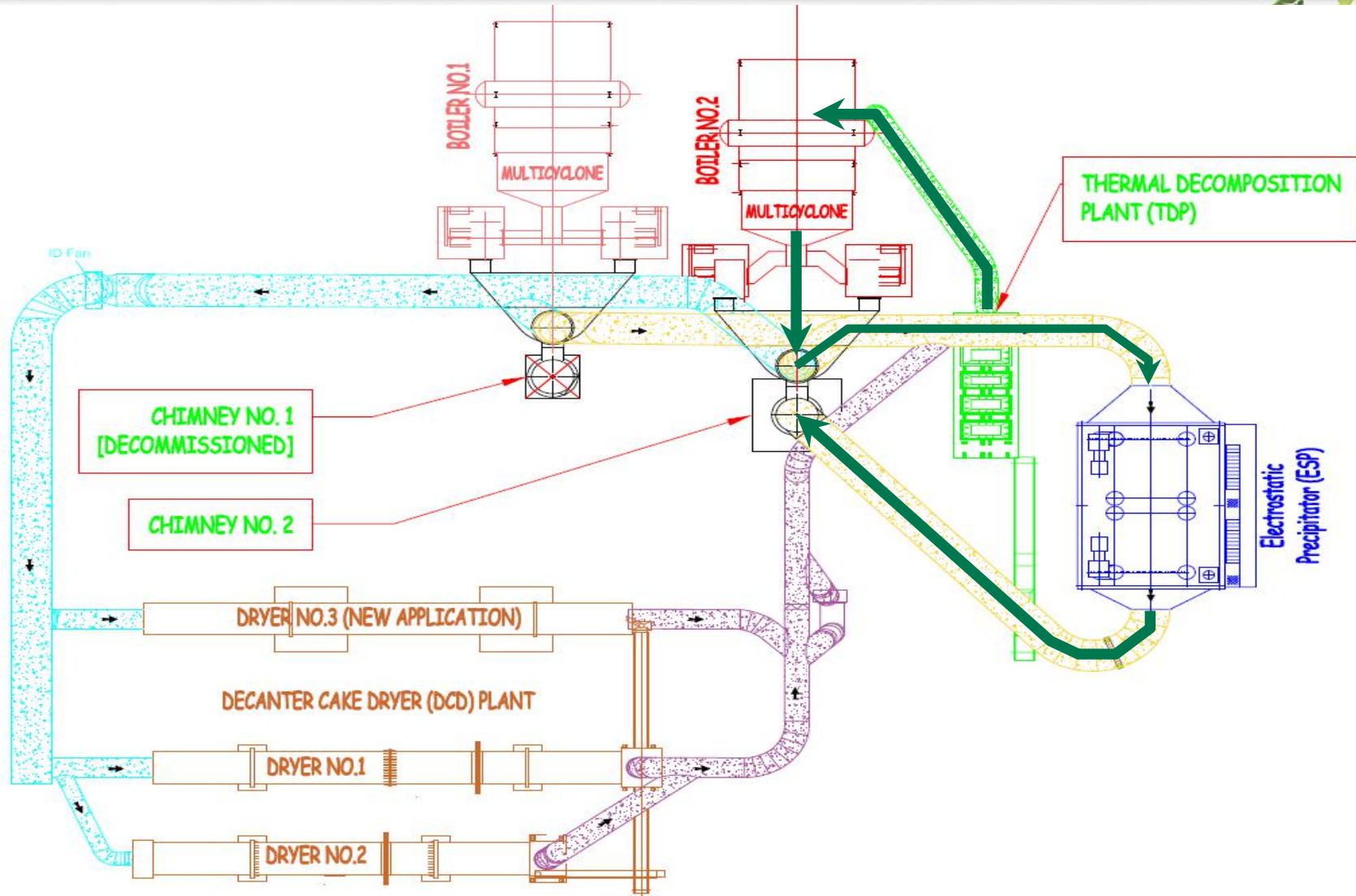
TDP

PILOT PLANT TEST RESULT

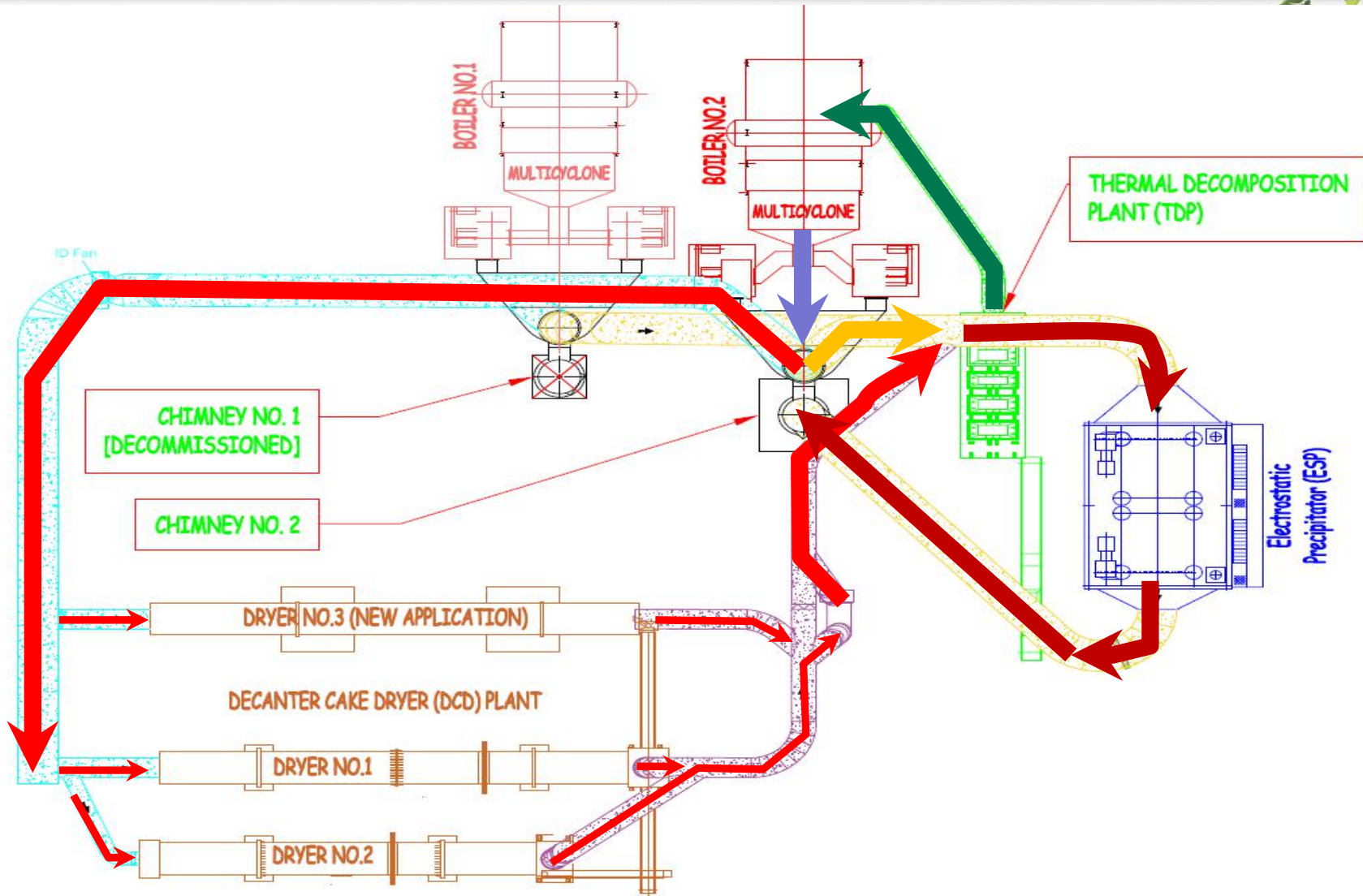
NORMAL CASE



NORMAL + TDP



NORMAL + TDP + DCD



STACK SAMPLING TEST

Client	MJM (PALM OIL MILL) SDN BHD (MJM PALM OIL MILL)		
Report Reference	SBTC/MJMPOM/22(01)		
Date	22nd April 2022		
Description	Units	B2-A Value (as given / measured)	B2-B Value (as given / measured)
Starting Time	-	09:30 hrs	11:00 hrs
Ending Time	-	10:30 hrs	11:36 hrs
Dust Particulate Emission	mg/Nm ³ , dry, @ 12% CO ₂	28.938	226.753
Standard Limit (Imposed by Department of Environment)	mg/Nm ³	400.0	400.0
Description	Units	B2-C Value (as given / measured)	B2-D Value (as given / measured)
Starting Time	-	12:00 hrs	13:00 hrs
Ending Time	-	12:36 hrs	13:36 hrs
Dust Particulate Emission	mg/Nm ³ , dry, @ 12% CO ₂	65.333	73.571
Standard Limit (Imposed by Department of Environment)	mg/Nm ³	400.0	400.0

EMISSION TEST RESULT

No.	Scenarios Description	Stack Sampling Result Dust Concentration (mg/m ³ @12%CO ₂)	Remarks
1	In Operation: Boiler 2 + ESP Not In Operation: TDP, DCD	73.571	NORMAL CASE (with ESP)
2	In Operation: TDP + Boiler 2 + ESP Not In Operation: DCD	65.333	NORMAL CASE + TDP
3	In Operation: TDP + Boiler 2 + DCD + ESP	29.938	NORMAL CASE + TDP + DCD
4	In Operation: TDP + Boiler 2 + DCD Not In Operation: ESP	226.753	NORMAL CASE (without ESP)

* Sampling & Tested by Accredited 3rd Party



FUTURE

PLAN FORWARD

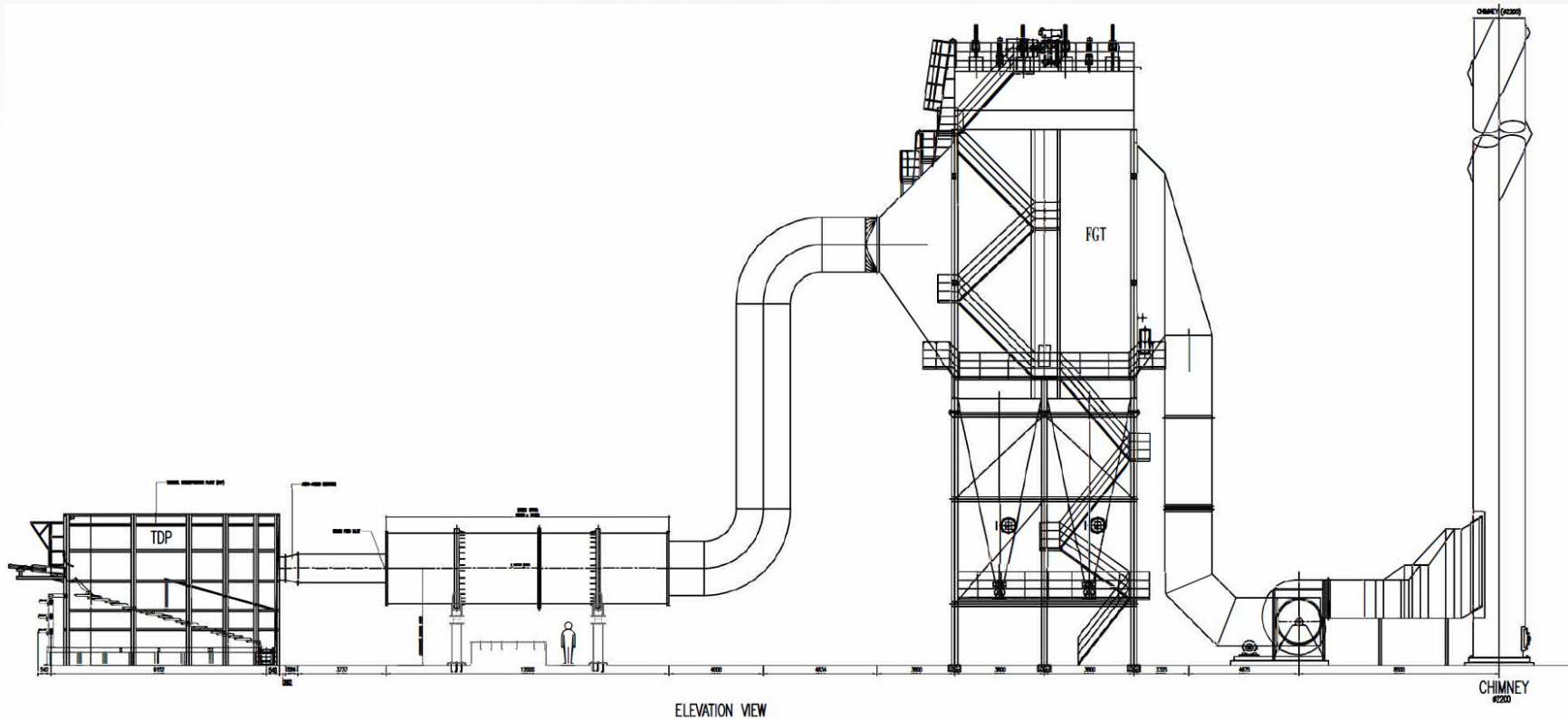


CONDITION of CONCEPT



- TDP **NEAR** to existing boiler
- IDF of existing boiler was **OVERSIZED**
- **SPACE** availability is sufficient
- Throughput **LIMITED** by existing IDF

FULLY STANDALONE TDP



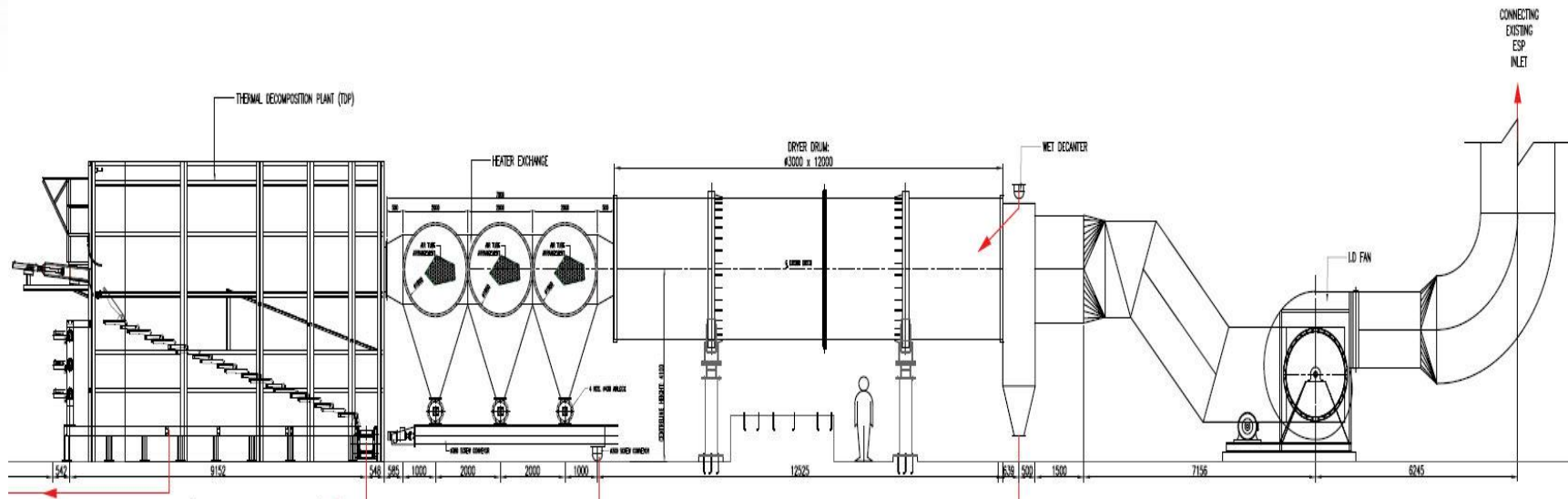
TDP

DCD

FGT

IDF

PARTIAL STANDALONE



TDP

HEX

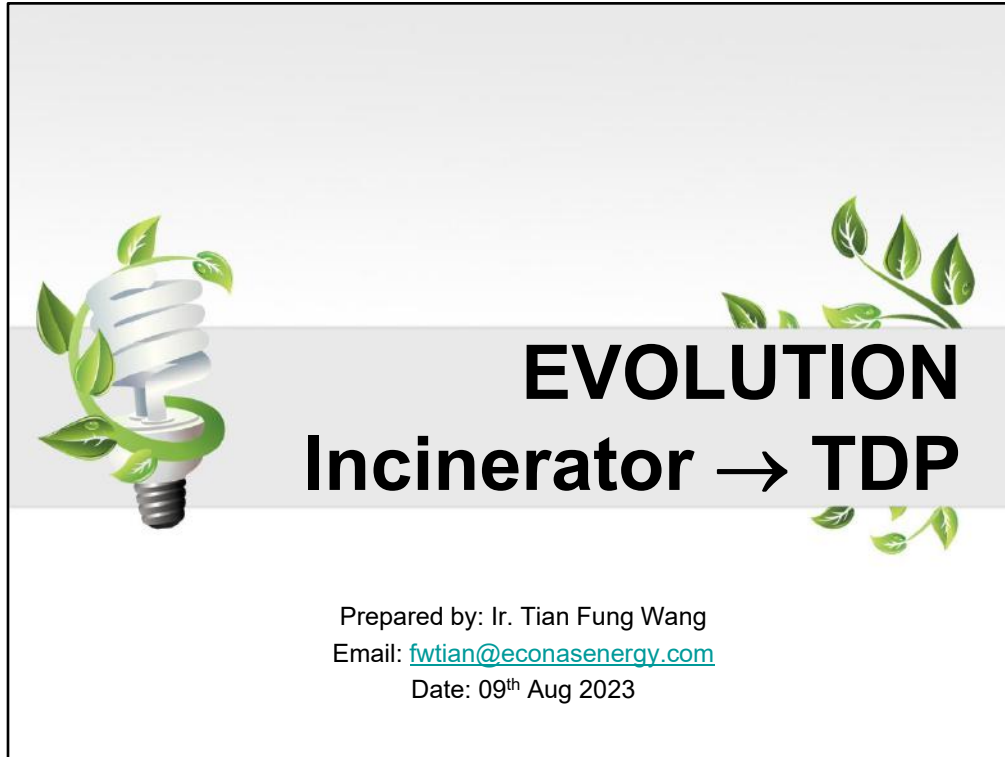
DCD

IDF

SARAWAK's EFB TREATED via SARAWAK INNOVATION



Thank You



Good afternoon, ladies & gentlemen.

My topic of discussion today is Evolution from Incinerator to TDP.

Honestly, I am not an expert in Palm Oil industry. My specialty is thermal treatment of municipal waste & hazardous waste.

My apology, if there is any error of facts in relation to Palm Oil industry, and please feel free to correct me.

Before I present in detail of TDP, I wish to explain a bit of my background which lead to the idea of evolving existing Natural Draft incinerator to TDP.



I had completed:

1. Thailand 1st Large Scale Municipal Waste Incineration Power Plant,
2. China, Xi An Municipal Waste to Fertilizer Plant,
3. Malaysia 1st Hazardous Waste Incineration Power Plant and
4. Indonesia 1st Large Scale Municipal Waste Gasification Power Plant.

All of these projects utilizing thermal treatment for waste disposal purpose.

Phuket 700TPD MSW Incineration Power Plant



China 300TPD MSW to Fertilizer Plant



Malaysia 100TPD SW Incineration Power Plant



Surabaya 750TPD MSW Incineration Power Plant





Nowadays, myself and partners are in the mid of developing Malaysia 3rd Scheduled Waste treatment center in Johor mainly to serve industry at southern part of Malaysia, generally serving whole Malaysia.

From the experience of municipal waste & hazardous waste incineration, it led to the idea of implementing the high efficiency combustion concept in Empty Fruit Bunch treatment for Palm Oil industry.



From my understanding, most of Sarawak Palm Oil Mill facing several challenges such as:

1. Empty Fruit Bunch disposal using low combustion efficiency natural draft incinerator
2. Difficulty in disposal of wet decanter cake
3. Enforcement of Environmental Quality Clean Air Regulations 2014

Empty Fruit Bunches



Wet Decanter Cake



EQ CAR 2014

Obligation to comply

4. (2) An owner of every existing premises, including that which is not subject to any condition on limit values for air pollutants whether on the licence issued or approval granted for the operation of the existing facility, shall, on or before the expiry of five years from the date on which these Regulations come into operation, take such measures as may be necessary to comply with the opacity and limit values as specified in regulations 12 and 13.

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SECOND SCHEDULE

[Regulation 13]

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	Coal	Sulphur content < 1% (per weight)
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		Residues from wood-based industries: without wood preservatives

EQ CAR 2014

The CO₂ reference content is 12%

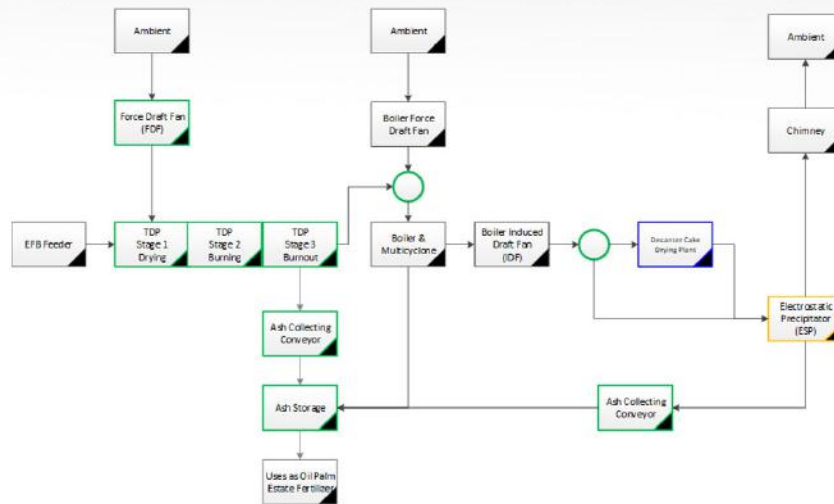
Fuel type	Pollutant	Limit value	Monitoring
Solid	Total particulate matter (PM) Where dust load emitted: (a) > 0.44 < 1.0 kg/h (b) ≥ 1.0 < 1.5 kg/h (c) ≥ 1.5 < 2.0 kg/h (d) ≥ 2.0 < 2.5 kg/h ⁰ (e) ≥ 2.5 kg/h	150 mg/m ³	Once/year 2 times/year 3 times/year 4 times/year Continuous*
	Carbon monoxide (CO)	1000 mg/m ³	Periodic

*Averaging time for continuous monitoring is 30 minutes



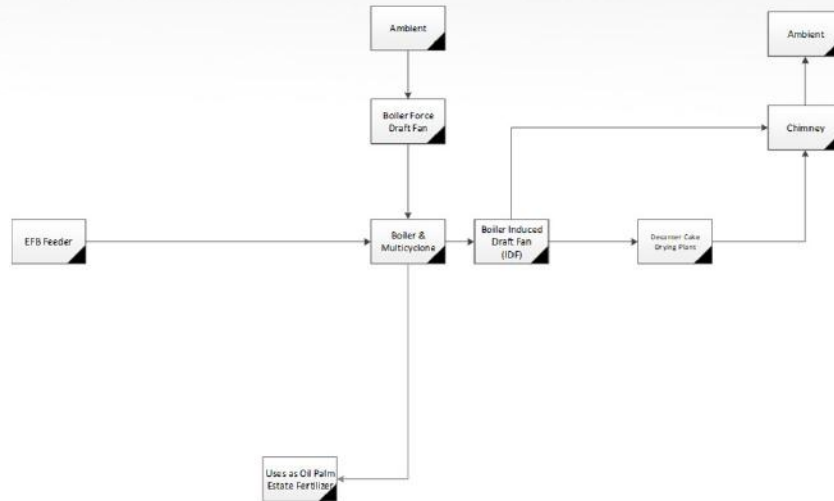
Due to the above, I was given a task by my brother to propose a high combustion efficiency concept in disposing EFB. Thus, it come to the innovation of TDP known as Thermal Decomposition Plant.

TDP TRIAL @ MJM



We had completed a Pilot Plant in MJM Palm Oil Mill by retrofitting the current Boiler set up to incorporate TDP into the overall process flow. Basically, we added a high efficiency combustion chamber that is able to burn 100% EFB couple with the current boiler operation mainly for EFB disposal. From the Pilot Plant, we found that the Ash generated consist of 25-30% potassium content which can be used as fertilizer.

ORIGINAL SET UP @ MJM



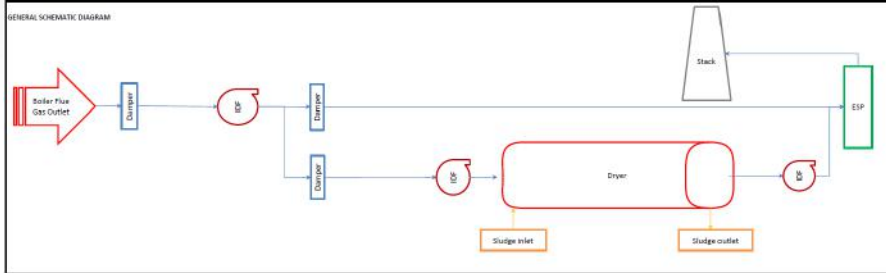
TDP CALCULATION

1 INPUT						
1.1 Ultimate Analysis						
Element	C	H	O	N	S	Cl
Percentage	36.97%	5.12%	33.52%	0.34%	0.35%	0.00%
1.2 Proximate Analysis						
Element	Moisture	Ash	Combustible	Density	HHV, kJ/kg	
Percentage	20.00%	3.70%	76.30%	0.50	14,794	
1.3 Throughput						
FFB Throughput	=	70 t/h				↓
EFB: FFB Ratio	=	23%				↓
EFB Throughput	=	16.1 t/h (Before press)				↓
Moisture Content	@	75% [Based on Test Report]				↓
Throughput	=	4.83 t/h (After drying)				↓
Moisture Content	@	20% [Design to control]				↓
	=	4,830 kg/h				↓
2 CALCULATION						
2.1 CALORIFIC VALUE						
2.1.1 LHV = $81C + 246H + 26S - 26O - 6W$						
	=	3,273 kCal/kg				↓
	=	13,700 kJ/kg				↓
Total Heat Output	=	66 GJ/h				↓
2.1.2 HHV = LHV + 600 (W + 9H)						
	=	3,669 kCal/kg				↓
	=	15,360 kJ/kg				↓
						< 5%
2.2 AIR REQUIREMENT						
2.2.1 Excess air factor = 1.8						
2.2.2 Air Required, L_a = $[8.89C + 26.7H + 3.33S - 3.33O] \times 10^{-2}$						
	=	3.55 Nm ³ /kg				
	=	30,867 Nm ³ /h				
2.2.3 Air Required, L_a = $[11.6C + 34.78H + 4.35S - 4.35O] \times 10^{-2}$						
	=	4.63 kg/kg				
	=	40,236 kg/h				
2.3 FLUE GAS						
2.3.1 Wet Flue Gas, L_w = $(m - 0.21)L_a + 1.867C + 0.7S + 0.8N + 11.2H + 1.24W + 0.62Cl$						
	=	7.16 Nm ³ /kg				
	=	34,594 Nm ³ /h				
2.3.2 Air Moisture Content						
2.3.2.1 Content = 1.5%						
2.3.2.2 L_m = 0.0959 Nm ³ /kg						
2.3.3 Dry Flue Gas (Flow) = $L_w - L_m - W - 9H$						
	=	6.41 Nm ³ /kg				
	=	30,938 Nm ³ /h				
2.3.4 Dry Flue Gas (Mass) = $(m - 0.2)L_a + 3.667C + 2S + N + 9H + W + 1.03Cl$						
	=	7.71 kg/kg				
	=	37,229 kg/h				

Normal Condition		
P_1	1	- Pa
V_1	34,594	Nm ³ /h
T_1	0	°C
Actual Condition		
P_2	-	- Pa
V_2	116,961	m ³ /h
T_2	650	°C

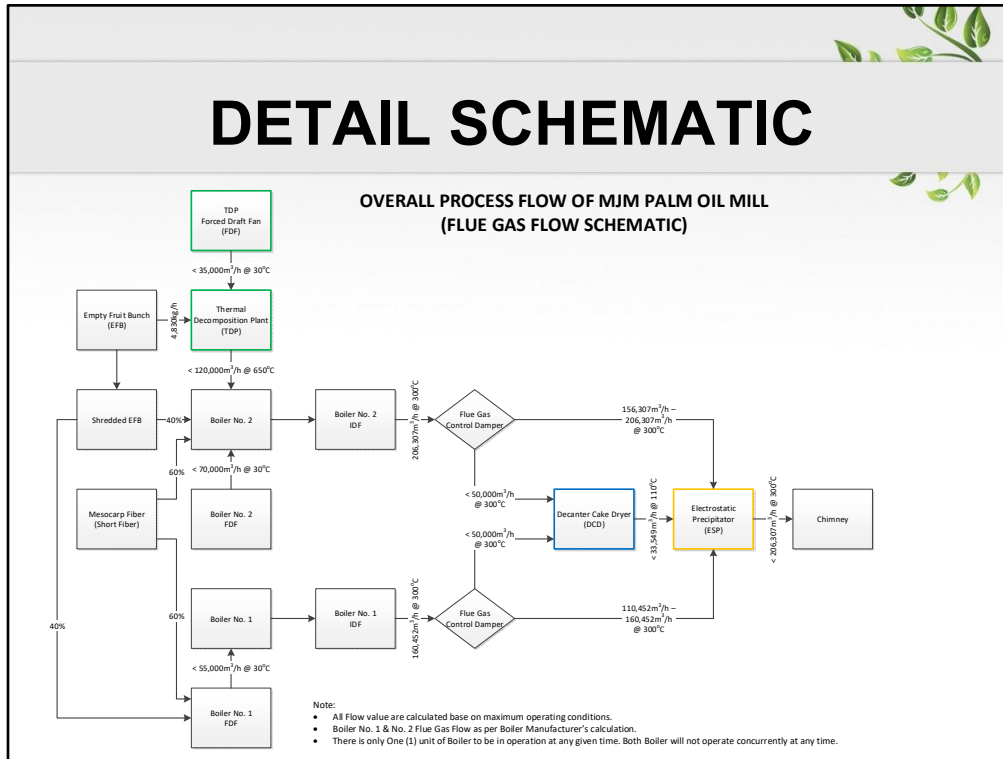
Here is calculation for TDP & Dryer during the design stage as it is important because the whole process was interlinked.

DRYER CALCULATION



SLUDGE DRYING PROCESS		FLUE GAS DRYING PROCESS	
MASS BALANCE		MASS BALANCE	
INLET	OUTLET	INLET	OUTLET
Mass flowrate Moisture content Temperature Dry matter flowrate Water content	1,111 kg/h Moisture content Temperature Water content	300 °C Relative Humidity Enthalpy Humidity Ratio Specific Volume Moisture per m ³ flow	Estimated 110 °C 20.00% RH @ 110 °C 782.95 kJ/kg 218.28 1.52 1.510 m ³ /kg 0.1637 0.1343 kg/m ³ Flow rate required 35,052
ENERGY BALANCE		ENERGY BALANCE	
ASSUMPTION	CALCULATION	INLET CONDITION	OUTLET CONDITION
Specific heat of water Latent heat of water Specific heat of sludge	Water evaporated Energy to heat up water Energy to heat up sludge Energy to evaporate water Total energy	300 °C Specific Energy Relative Humidity Humidity Ratio	Estimated 110 °C 782.95 kJ/kg 20.00% 1.52 1.510 m ³ /kg Without superheating Humidity Ratio Enthalpy Net Energy differences Energy per m ³ flow Flow rate required
COLOUR NOTES			
Heat assumption			
Value from Psychrometric Chart			

DETAIL SCHEMATIC



Hot flue gas from TDP channeled into Boiler may help to reduce the need of burning PKS in the boiler.

Since MJM Plant also facing Wet Decanter cake issue, the hot flue gas from boiler was used to dry up the wet decanter cake for other purpose which give additional income stream to the Palm Oil Mill.

TDP CONSTRUCTION



Here are some photos of TDP during construction.

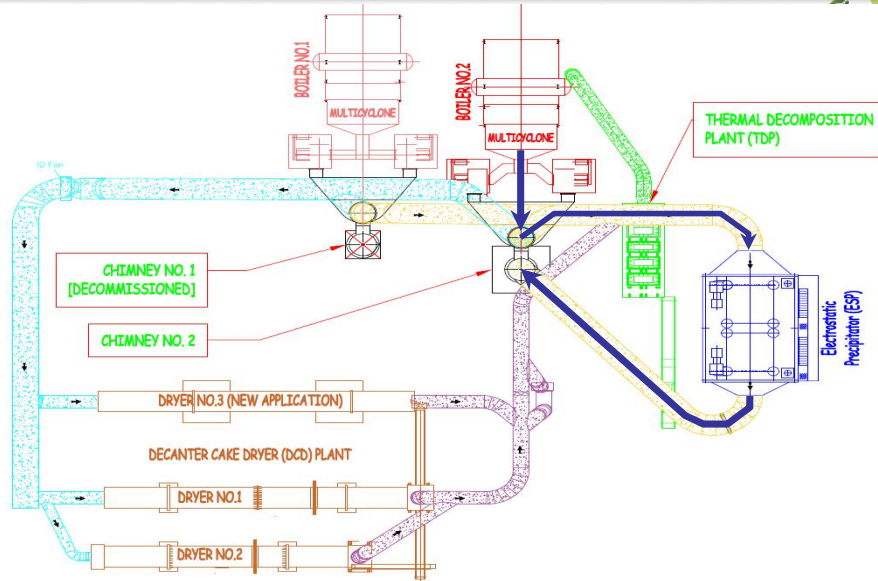


Please allow me to present you the Pilot Plant third party sampling result on TPM for your reference.

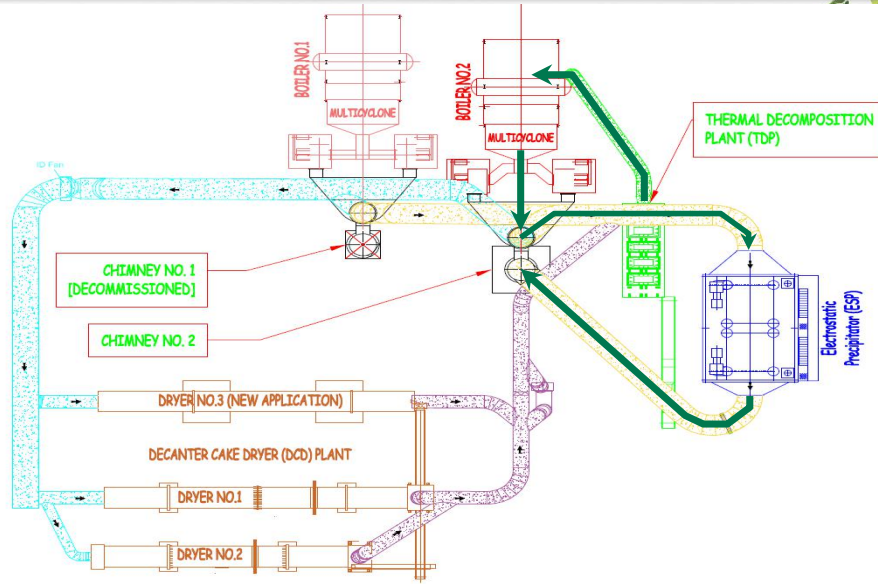
Since the plant consist of existing Boiler, TDP and DCD, we categorize the operating condition as

1. Normal Case – Only Boiler is in Operation
2. Normal Case + TDP – Boiler & TDP is in Operation
3. Normal Case + TDP + DCD – Boiler, TDP & DCD are all in operation

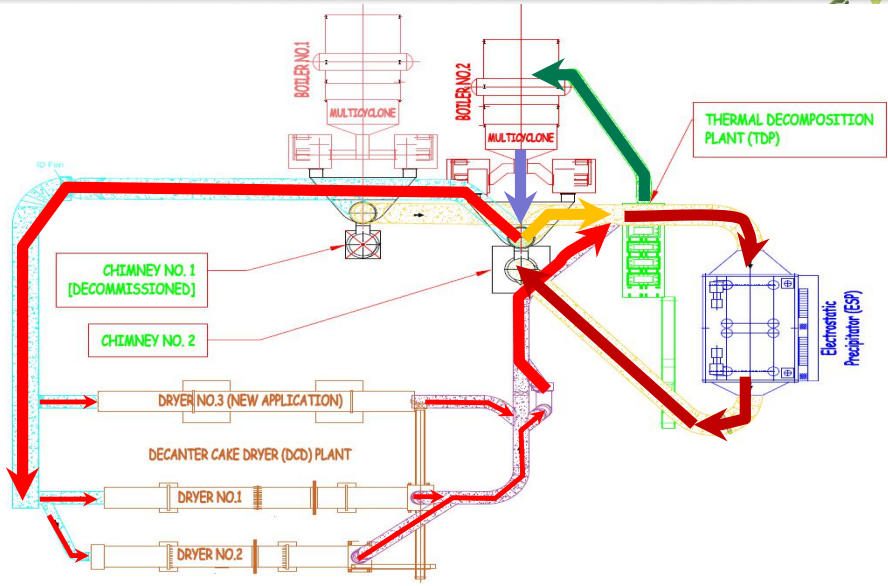
NORMAL CASE



NORMAL + TDP



NORMAL + TDP + DCD



STACK SAMPLING TEST

Client	MJM (PALM OIL MILL) SDN BHD (MJM PALM OIL MILL)		
Report Reference	SBTC/MJMPOM/22(01)		
Date	22 nd April 2022		
Description	Units	B2-A Value (as given / measured)	B2-B Value (as given / measured)
Starting Time	-	09:30 hrs	11:00 hrs
Ending Time	-	10:30 hrs	11:36 hrs
Dust Particulate Emission	mg/Nm ³ , dry, @ 12% CO ₂	28.938	226.753
Standard Limit (Imposed by Department of Environment)	mg/Nm ³	400.0	400.0
Description	Units	B2-C Value (as given / measured)	B2-D Value (as given / measured)
Starting Time	-	12:00 hrs	13:00 hrs
Ending Time	-	12:36 hrs	13:36 hrs
Dust Particulate Emission	mg/Nm ³ , dry, @ 12% CO ₂	65.333	73.571
Standard Limit (Imposed by Department of Environment)	mg/Nm ³	400.0	400.0

Third party sampling was done for these operating conditions.

EMISSION TEST RESULT

No.	Scenarios Description	Stack Sampling Result Dust Concentration (mg/m ³ @12%CO ₂)	Remarks
1	In Operation: Boiler 2 + ESP Not In Operation: TDP, DCD	73.571	NORMAL CASE (with ESP)
2	In Operation: TDP + Boiler 2 + ESP Not In Operation: DCD	65.333	NORMAL CASE + TDP
3	In Operation: TDP + Boiler 2 + DCD + ESP	29.938	NORMAL CASE + TDP + DCD
4	In Operation: TDP + Boiler 2 + DCD Not In Operation: ESP	226.753	NORMAL CASE (without ESP)

* Sampling & Tested by Accredited 3rd Party

We found that,

1. ESP is able to achieve 73ppm at Normal case as compare to 226ppm without ESP.
2. During TDP in operation, the dust particulate emission reduces a little bit as the combustion had been shifted in front gives more room for dust settling.
3. During DCD in operation, the dust particulate emission reduces significantly because temperature of the flue gas was dropping and the ESP now become oversized in terms of flow rate and yield better efficiency.



Next, I wish to share some of the plan forward in treating EFB via TDP.



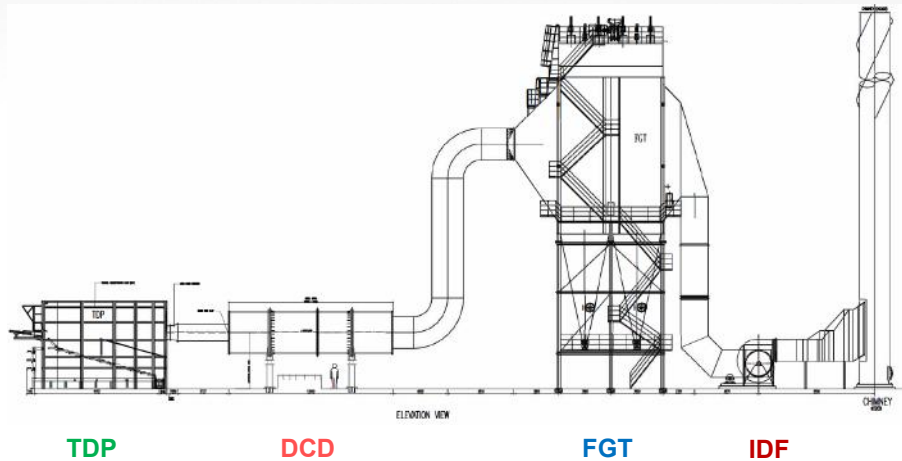
CONDITION of CONCEPT

- TDP **NEAR** to existing boiler
- IDF of existing boiler was **OVERSIZED**
- **SPACE** availability is sufficient
- Throughput **LIMITED** by existing IDF

Since the TDP in Pilot Plant was couple with existing boiler, there are some limitations in scaling up of this concept:

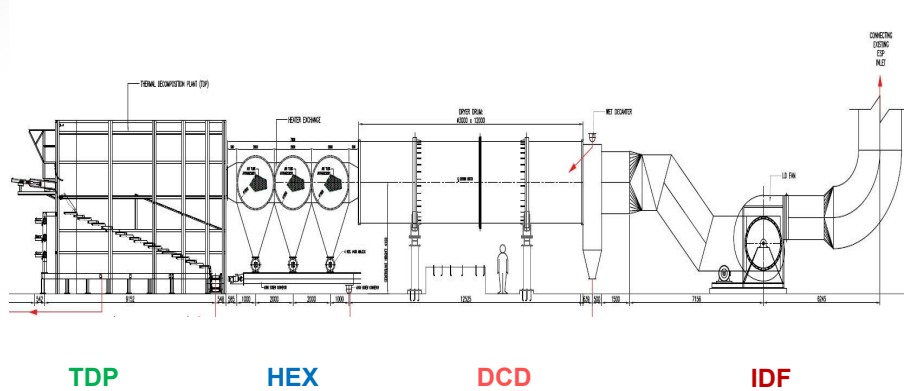
1. In terms of layout, TDP need to be near to existing Boiler
2. In terms of capacity, IDF of existing boiler need to be oversized or still have room for speeding up.
3. Normally, there is no space beside existing boiler for most of the Palm Oil Mill.
4. Throughput of TDP will be limited by the Boiler IDF as it relying on IDF in controlling the negative pressure in combustion chamber.

FULLY STANDALONE TDP



Due to the above limitation, the solution is to have a fully standalone unit like this OR

PARTIAL STANDALONE



partially standalone unit like this where the throughput of EFB disposed was not limited.



Last but not least, I think we need to put effort to resolve our own challenges within Sarawak because the nature of the commercial environment in Sarawak might be different from the other states.

For example, other states in Malaysia may apply Feed In Tariff for EFB Power Plant and get good revenue while generating electricity from EFB and export to the national grid. Unfortunately, Feed In Tariff in Sarawak might not be that attractive as compare to other states for the moment. Thus, converting EFB to fertilizer probably give better ROI in Sarawak.

This ends my today's presentation. Thank you for your passion and I wish you all the best.